## SUPPLEMENTAL INSTRUMENTATION APPENDIX

TO PERIODIC INSPECTION REPORT NO. 4

BUFFUMVILLE LAKE

CHARLTON, MASSACHUSETTS

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Standards for Settlement Surveys

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#### BUFFUMVILLE LAKE

## INSTRUMENTATION FOR SAFETY EVALUATION

#### 1. Project Performance.

The project's condition is judged to be good based on visual observations and instrumentation data. The crest monument data indicates that typically 0 to 1 inch of settlement has taken place at the dam since 1976 and 0 to 2.5 inches of horizontal movement has taken place at the dam since 1978. Larger horizontal movements (10.0 inches at A, 4.6 inches at POL-1 and 24.0 inches at POC-2) and larger settlement (7.8 inches at POL-9) were noted but are attributed to survey errors. A study to determine the number and location of piezometers needed at Buffumville Dam was performed in FY91. It recommended that two double piezometers and one single piezometer be installed at the dam in FY95 as discussed in Section 5 of this report.

### 2. Project Description.

a. <u>General</u>. The project is one unit of a system of six reservoirs and dams situated in the Thames River Basin, Connecticut and Massachusetts. The dam is located approximately 1.3 miles upstream of the French and Little Rivers confluence on the Little River in Charlton, Massachusetts as shown on Plate 1. The reservoir is located in the towns of Oxford and Charlton, Worcester County, Massachusetts. The major project features are an earth and rockfill dam, a combined spillway and outlet, and an earth and rockfill dike. Project construction was started September 1956 and was completed June 1958.

### b. Geology and Foundations.

(1) <u>Topography and Geology</u>. Little River is located near the eastern border of the maturely dissected New England Upland. The area has low to moderate relief which has been altered by glaciation. Rounded hills and ridges form the edges of relatively, wide, flat valleys. Steep, rough, rocky slopes and channels sometimes dissect the generally rolling terrain.

A thin layer of clayey glacial till with boulders covers the hills in the area. Bedrock penetrates through the till on many of the hills. The valleys are filled with thicker layers of till and outwash materials which were deposited on the till when the glacier melted. The glacial filling of the valleys has changed the pre-glacial drainage paths so that many of the old valleys are blocked, some streams have been diverted, and many ponds and marshes occupy the wide valley bottoms. The present streams flow high above their pre-glacial channels due to the thick deposits of till and outwash. Bedrock is observed in the valleys only where streams have uncovered bedrock ridges or spurs on the sides of the old valleys.

The main valley of the Little River extends north to south like most of the valleys in the region. During the final stages of glaciation, the southward drainage path was blocked by ice and debris. Ponded water spilled over a low saddle at the eastern divide of the basin and the river cut its present eastward course along an old valley through the bedrock ridge. After the ice receded, the southward drainage path was still blocked by low deposits of glacial materials between Hayden Pond and Pierpoint Meadow Pond, so the river continued to flow eastward to the French River.

(2) <u>Dam Site</u>. The 0 to 60 foot thick overburden at the dam consists of outwash underlain by glacial till. The outwash is poorly to well stratified or lensed, loose to moderately compact sandy silt, silty sand, gravelly sand and sandy gravel. On the south side of the river, the outwash deposits are generally less than 10 feet thick except at the upstream end of the spillway where they are up to 20 feet thick. On the north side of the river, the outwash deposits are 5 to 10 feet thick along the crest of the ridge which runs under the centerline of the embankment. Downstream of the ridge, the outwash deposits tend to thin while upstream they are up to 20 feet thick. Near the north end of the dam, the outwash deposits become stratified silts and silty sands and increase to 40 feet in thickness.

Two phases of glacial till were observed below the glacial outwash. The upper phase is a looser, less impervious silty sand with cobbles and boulders. It was dropped in place by the receding glacier. The lower phase is a very compact, relatively impervious silty to clayey, gravelly sand with cobbles and boulders. It was deposited and compressed on the bedrock surface by actively moving ice. Both phases of the till are very variable in thickness and disappear around knolls and near the north abutment.

Exploration locations and details for the dam and appurtenant structures which give more details concerning the foundation materials are shown on Plates 2 and 3.

- (3) <u>Dike Site.</u> The foundation materials vary from compact glacial till at the east end of the dike to glacial outwash at the west end of the dike. The glacial till is primarily semi-pervious to impervious silty sand and gravel. The outwash materials are mainly semi-pervious silty gravels with minor amounts of pervious and semi-pervious silty sands. A marshy area exists immediately downstream of the dike and is attributed to seepage through the existing road embankment.
- (4) <u>Bedrock</u>. The bedrock under most of the foundation area is calcareous, quartz-mica schist. Granite occurs near the north end of the dam and at the north abutment. The schist is hard, fresh and broken by relatively few joints. Although the schistosity is generally well developed and the schist in many areas is phyllitic, the foliation planes are tight and the rock is considered sound and strong. The granite on the north abutment is gneissic and has occasional quartz veins and pegmatite zones. It is generally moderately hard and fresh, although some weathering has occurred along occasional joints.

(5) <u>Groundwater</u>. Groundwater levels measured before the construction of the dam were generally 10 to 20 feet below the surface. One exception was in the vicinity of Station 38+00 near the north end of the dam where surficial marshes and springs existed. More information pertaining to groundwater levels is shown on Plate 3.

## c. Dam and Appurtenant Structures.

- (1) <u>Dam</u>. The embankment of Buffumville Dam is a rolled earth fill which has a total length of 3,255 feet and a maximum height of 66 feet above the streambed. The limits of the embankment are shown on Plate 4. The embankment section, as shown on Plates 5, 6, and 7, consists of an impervious fill core with an upstream pervious fill zone, and downstream random fill zone. The upstream slope is covered with a 2-foot layer of stone slope protection underlain by a 1-foot layer of gravel bedding while the downstream slope is covered with a 1-foot layer of stone slope protection underlain by one-half foot layer of gravel bedding. The upstream slope is 1 vertical on 2.5 horizontal except below elevation 500 feet National Geodetic Vertical Datum (NGVD) where a 3-foot layer of stone slope protection underlain by 1 foot gravel bedding was placed. The downstream slope is 1 vertical on 2 horizontal. Seepage through the embankment is controlled by an impervious fill cutoff to glacial till, a downstream pervious blanket and a downstream toe drain.
- (2) <u>Outlet Works</u>. The outlet works consist of an inlet channel, an inlet structure, three conduits, an outlet structure and an outlet channel as shown on Plate 8. The inlet channel is a stone-lined earth cut that is 22 feet wide at the bottom and approximately 520 feet long. It leads up to a 30 foot long U-shaped concrete inlet structure which is founded on bedrock. Three 3-foot wide by 4.5 foot high by 45 foot long concrete conduits founded on bedrock connect the inlet structure to the outlet structure. The outlet structure is a 45 foot long U-shaped concrete structure which is founded on bedrock. The outlet channel is a stone-like earth cut that is 20 feet wide at the bottom and approximately 1,000 feet long.

There are three 3 foot by 4.5 foot slide gates in the outlet works. A permanent pool is retained at Elev. 492.5. Flood operation is required during storm events because the gates are manually operated.

- (3) <u>Spillway.</u> A chute spillway is located on the center section of Buffumville Dam as shown on Plates 4 and 8. It is separated from the embankment by the two retaining walls. The weir has a 220-foot long concrete ogee section which is founded on rock. The weir crest is at elevation 524 feet NGVD. The spillway approach and discharge channels were excavated mainly in earth. The approach channel is approximately 175 feet long, 230 feet wide and has a bottom elevation of 515 feet NGVD. The discharge channel is approximately 1,000 feet long, varies in width from 22 feet to 100 feet and has a bottom elevation of 485 feet NGVD. Two 100-foot by 100-foot stilling basins with bottom elevations of 485 feet NGVD are located at the upstream end of the discharge channel.
- (4) <u>Dike.</u> The dike embankment is 610 feet long and has a maximum height of 15 feet (crest elevation is 539 feet NGVD) as shown on Plate 9. It has an impervious fill core which is protected by one foot of

stone protection underlain by one foot of gravel bedding upstream and grass downstream. A 6-foot wide impervious fill cutoff trench was provided to reduce seepage under the dike. Foundation treatment for the dike was limited to stripping topsoil.

## 3. Existing Instrumentation.

Nineteen crest monuments were installed at Buffumville in 1976. They are located on the crest of the dam as shown on Plates 10, 11 and 12. The crest monuments are standard brass disks that have been set in 3-foot long concrete filled pipes. They typically are set flush with the existing bituminous pavement on the crest of the dam. It was noted that they were loose and could be moved up to 0.25 inches horizontally during the January 1989 periodic inspection.

The crest monuments are surveyed from Control Points B-127, R2-D2, J, I, H, G and F which are shown on Plates 11 and 12. The control points are standard brass disks that have been set in outcrops or concrete filled sonatubes.

# 4. Data Collection, Interpretation and Evaluation.

The crest monuments were surveyed June 1976, May 1978, August 1984 and January 1989. The results of the surveys are shown on Plates 11 and 12. Each survey was tied to the Massachusetts Lambert Grid System. Distances were measured using a tape for the 1976 survey and using electronic distance measuring equipment for the 1978, 1984 and 1989 surveys. Standards presently being used for settlement surveys are included in Attachment No. 1.

Plate 12 shows graphical representation of the survey results. The observed vertical movements from 1976 to 1989 typically varied between 0 and 1 inch and averaged 0.7 inches. The observed horizontal movements from 1978 to 1989 typical varied between 0 and 2.5 inches and averaged 1.2 inches. Larger movements (10 inches horizontal at A, 4.6 inches horizontal at POL-1, 24 inches horizontal at POL-2 and 7.8 inches vertical at POL-9) were observed, but they are attributed to survey error. There seems to be no trend in the horizontal movements and a small downward trend in the vertical movements.

### 5. <u>Conclusions and Recommendations</u>.

a. <u>General</u>. The geotechnical instrumentation at Buffumville Lake Dam presently consists of nineteen crest monuments. It is recommended that two double piezometers and one single piezometer be installed in FY95 to monitor porewater pressures in the embankment as discussed in Section 5d.

#### b. <u>Crest Monuments</u>.

(1) <u>General.</u> Maximum horizontal and vertical movements of 2.5 inches and 1 inch have been observed at Buffumville Dam. The maximum movements appear reasonable to expect at a project of this type.

- (2) <u>Schedule.</u> Crest monument surveys at Buffumville Dam are scheduled once every five years to coincide with the periodic inspection schedule. The next scheduled survey is to be performed in 1994. Thesurvey schedule will be adjusted if field evidence of embankment movement occur or unusual readings are obtained from a survey.
- (3) Evaluation of Adequacy. The number of crest monuments and current standards for surveying them at Buffumville Dam are adequate. A Global Position Systems Survey such as NAVSTAR which can detect movements of less than 0.2 inches (ETL 1110-1-133) will be implemented if it is cost effective.
- c. <u>Strong Motion Instruments</u>. Strong motion instruments have not been installed at Buffumville Dam because the risk of a large earthquake at the project site is relatively low, and the cost to install, read, and maintain strong motion instruments is high.
- d. <u>Piezometers</u>. The installation of piezometers is needed at Buffumville Dam to monitor the phreatic line within the dam embankment and foundation pore pressures. Two double piezometers and one single piezometer are recommended as shown on Plate 13. They should be located at approximately Station 18+00, 32 feet upstream, 25 feet downstream and 114 feet downstream from the dam centerline. The piezometers will measure piezometric levels in the impervious fill core (PZ-1A), the earth foundation (PZ-11B and PZ-21B), the random fill zone (PZ-2A), and the downstream pervious blanket (PZ-3) of the dam. The estimated cost for the installation of the proposed piezometers is \$40,000. The estimated cost includes associated engineering, supervision and administration. The work should be scheduled and budgeted for FY95.

The following standards and procedures are employed for Crest Monument Surveys at Buffumville Dam.

## STANDARDS FOR SETTLEMENT SURVEYS

- 1. Control points are stamped brass disks preferably set in a ledge area. Where no ledge is available, they are set in concrete bounds placed flush with the ground.
- 2. Control points are set in areas such that the maximum possible number of crest monuments on the dam are visible.
- 3. Control points are tied into four reference points by distance. This provides a check each time they are occupied for settlement surveys or allow them to be replaced if found to be destroyed.
- 4. Distances are read and recorded between settlement bounds. Both distance and angle are read and recorded from the control points that are being occupied to locate each settlement bound on the dam.
- 5. In locating each settlement bound, a control point will be occupied setting 0-00'-00" (referenced line of site) on a second control point, reading and recording both interior and exterior angle closure, along with distances through each settlement bound located on the dam. Each settlement bound is located from a minimum of two control points. These locations are third order, class II survey with relative accuracies of not less than 1 part in 5,000.
- 6. Levels are run from control points through each settlement bound on the dam with a return run back into the control points to check the elevation closure on the run. Closure tolerance should be no greater than 0.05°. These levels are third order, class I survey with relative accuracies not less than 1 part in 10,000.
- 7. Crest monument surveys are performed using Topcon EDM Total Stations and recording both horizontal angles and horizontal distances.

## PROCEDURE FOLLOWED FOR SETTLEMENT SURVEYS

The horizontal and vertical monitoring plan for settlement bound movement points employed a combination of triangulation and trilateration angle and distance techniques to survey the control network. Control points, in the form of stamped brass disks, were placed off the dam structure in areas from which the entire length of the dam is visible. Settlement bounds themselves, with stamped brass disks, were placed on the dam structure in a location that is clearly visible from the control points. Horizontal coordinates of the control points are based on the State Plane Coordinate System. Elevations of the control points are based on the National Geodetic Vertical Datum (NGVD). Control points are occupied utilizing an EDM Total Station; observed distances and angles (interior and exterior angles), between control points and settlement bound establishing permanent bench marks. Standard leveling techniques are followed. Levels are double run and the means of the front and back runs were computed and recorded.

#### DATA ADJUSTMENT

A combination of triangulation and trilateration surveying techniques are applied. Each crest monument is located from two control points and two sets of coordinates are calculated using adjusted field angles and compliments and EDM distances. The two sets of coordinates are averaged to give a net result. The averaged coordinates are then established on each settlement bound for use in determining shifts in the dam surface structure over a period of years by comparing repetitive surveys.























